

# COUPLING SELECTION BASED ON OPERATING FACTORS

## Coupling types

### Lamina couplings

**RADEX®-N** Steel lamina coupling (see page 164)



- Torsionally rigid
- Backlash-free
- Maintenance-free
- Compact dimensions
- Single-cardanic or double-cardanic
- All-steel

**RIGIFLEX®-N** Steel lamina coupling (see page 164)



- Torsionally rigid
- Backlash-free
- Maintenance-free
- Double-cardanic
- All-steel
- Coupling in accordance with API 610, API 671 optionally

**RIGIFLEX®-HP** High-performance steel lamina coupling (see page 164)



- Torsionally rigid
- Backlash-free
- Maintenance-free
- Double-cardanic
- All-steel
- Coupling design as per API 671

### Pin & bush couplings

**REVOLEX® KX-D** Flexible pin & bush coupling (see page 73)



- Flexible
- Maintenance-free
- Fail-safe
- Compact dimensions
- Axial plug-in

### Gear couplings

**GEARex®** All-steel gear coupling (see page 82)



- Torsionally rigid
- Fail-safe
- Compact dimensions
- Double-cardanic
- High power density
- All-steel

## Terminology of coupling selection

Description	Symbol	Definition or explanation
Rated torque of coupling [Nm]	$T_{KN}$	Torque that can be continuously transmitted over the entire permissible speed range.
Maximum torque of coupling [Nm]	$T_{K \max}$	Torque that can be transmitted as dynamic load $\geq 10^5$ times or $5 \times 10^4$ as vibratory load, respectively, over the entire operating life of the coupling
Vibratory torque of coupling [Nm]	$T_{KW}$	Torque amplitude of the permissible periodical torque fluctuation with a frequency of 10 Hz and a basic load of $T_{KN}$ or dynamic load up to $T_{KN}$ , respectively
Rated torque of machine [Nm]	$T_N$	Stationary rated torque on the coupling
Peak torque of machine [Nm]	$T_S$	Peak torque on the coupling

Description	Symbol	Definition or explanation
Engine power [kW]	P	Rated power of drive
Speed [rpm]	n	Rated speed of engine
Starting factor	$S_Z$	Factor taking into account load caused by starting frequency per hour
Direction factor	$S_R$	Considers the torsional direction
Temperature factor	$S_t$	Temperature factor – Factor considering the lower loading capacity particularly in case of increased temperatures.
Operating factor	$S_B$	Factor considering the different demands on the coupling dependent on the application.

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## Factors

Temperature factor $S_t$								
	-30 °C +30 °C	≤ +40 °C	≤ +60 °C	≤ +80 °C	≤ +150 °C	≤ +200 °C	≤ +230 °C	≤ +270 °C
REVOLEX® KX-D	1,0	1,2	1,4	1,8	-	-	-	-
GEARex®	1,0	1,0	1,0	1,0	-	-	-	-
RADEX®-N, RIGIFLEX®-N, RIGIFLEX®-HP	1,0	1,0	1,0	1,0	1,0	1,10	1,25	1,43

  

Starting factor $S_z$				Direction factor $S_R$	
Starting frequency per hour	<10	<25	<50	Same torsional direction	1,0
$S_z$	1,0	1,2	1,4	Alternating torsional direction	1,7

  

Operating factor $S_B$			
Application		Application	
<b>Construction machines</b>		<b>Mixers</b>	
Manoeuvre winches	1,50 – 2,00	Constant density	1,75 – 2,25
Swing gears	1,50 – 2,00	Variable density	2,00 – 2,50
Miscellaneous winches	1,50 – 2,00	<b>Grinders</b>	
Filters, cable winches	1,75 – 2,25	Centrifugal mills	1,75 – 2,00
Multi-bucket excavators	1,75 – 2,25	Beater mills	1,75 – 2,00
Running gears (caterpillars)	1,75 – 2,25	Autogenous mills	1,75 – 2,00
Impellers	1,75 – 2,25	Hammer and ball mills	2,00 – 2,50
Cutter drives	2,00 – 2,50	<b>Food industry</b>	
Elevators	1,50 – 2,00	Sugarcane harvesters	1,25 – 1,50
<b>Conveyors</b>		Sugar-beet harvesters	1,25 – 1,50
Bucket elevators	1,50 – 2,00	Sugar-beet washing	1,25 – 1,50
Elevators	1,75 – 2,25	Kneading machines	1,75 – 2,00
Hauling winches	1,50 – 2,00	Sugarcane breakers	1,75 – 2,00
Apron conveyors	1,25 – 1,75	Sugarcane mills	1,75 – 2,00
Rubber belt conveyors (bulk)	1,25 – 1,75	<b>Oil industry</b>	
Boom plate bucket conveyors	1,25 – 1,75	Filter presses for paraffin	1,50 – 2,00
Rotary conveyors	1,50 – 1,75	Rotary furnaces	1,75 – 2,00
Steel plate conveyors	1,50 – 1,75	<b>Paper machines</b>	
Worm conveyors	1,25 – 1,50	Couch rolls	1,75 – 2,25
Steel belt conveyors	1,75 – 2,00	Calanders	1,75 – 2,25
Conveyors	1,75 – 2,00	Wet presses	1,75 – 2,25
Rubber belt conveyor (bulk)	1,75 – 2,00	<b>Pumps</b>	
Inclined lifts	1,75 – 2,00	Radial pumps	1,25 – 1,75
Shaking slides	2,00 – 2,25	Centrifugal pumps (light liquid)	1,50 – 2,00
<b>Generators</b>		Centrifugal pumps (viscous liquid)	2,25 – 1,50
Frequency converters	1,75 – 2,00	Gear and vane pumps	1,50 – 1,75
Generators	1,50 – 2,00	Piston pumps, plunger pumps and press pumps	2,00 – 2,50
<b>Rubber &amp; nylon industry</b>		<b>Agitators</b>	
Rubber calenders and rolling mills	1,25 – 2,00	Light liquid	1,25 – 1,50
Mixers	1,25 – 2,00	Viscous liquid	1,50 – 1,75
Extruders	1,25 – 2,00	Liquid with constant density	1,25 – 1,50
<b>Lifters/cranes</b>		Liquid with variable density	1,50 – 2,00
Bridge cranes for steel industry	2,00 – 2,25	<b>Textile industry</b>	
Cranes (heavy load operation)	2,00 – 2,25	Winders	1,25 – 1,75
Running gears	1,75 – 2,25	Printing and dyeing machines	1,25 – 1,75
Lifting gears	1,75 – 2,25	Shredders	1,50 – 2,00
<b>Woodworking machinery</b>		<b>Fans, ventilators and blowers</b>	
Planing machines	1,50 – 1,75	Light-weight fans	1,25 – 1,75
Barking machines	1,75 – 2,00	Large blowers	1,75 – 2,50
Saw frames	1,75 – 2,00	Centrifugal fans	1,25 – 1,50
<b>Compressors</b>		Industrial fans	1,25 – 1,50
Centrifugal compressors	1,50 – 2,00	Rotary blowers	1,25 – 1,75
Rotary compressors	1,50 – 2,00	Fans (axial / radial)	1,25 – 1,75
Turbo compressors	2,00 – 2,50	Fans for cooling towers	1,50 – 2,00
Piston compressors	2,50 – 3,00	<b>Wastewater treatment plants</b>	
<b>Metal industry</b>		Rakes	1,25 – 1,50
Wire pulls	1,25 – 1,50	Worm pumps	1,25 – 1,50
Winders	1,25 – 1,50	Concentrators	1,25 – 1,50
Winding drums	1,50 – 2,00	Mixers	1,25 – 1,75
Wire drawing machines	2,00 – 2,50	Aerators	1,75 – 2,00
Plate shears	2,00 – 2,50	<b>Machine tools</b>	
Block pushers	2,00 – 2,50	Scissors	1,50 – 2,00
Blooming and slabbing	2,00 – 2,50	Dressing rollers	1,50 – 2,00
De-scalers	2,00 – 2,50	Bending machines	1,50 – 2,00
Hot-rolling mill	2,00 – 2,50	Hole punching machines	1,75 – 2,50
Cold rolling mills	2,00 – 2,50	Levelling machines	1,75 – 2,50
Billet shears	2,00 – 2,50	Hammers	1,75 – 2,50
Plugging machines	2,00 – 2,50	Presses	1,75 – 2,50
Continuous casting machines	2,00 – 2,50	Forging presses	1,75 – 2,50
Shifting devices	2,00 – 2,50	<b>Other</b>	
Application	2,00 – 2,50	Equipment for transport of persons	2,00 – 2,50
Roller tables (heavy-weight)	2,00 – 2,50	Rock crushers	2,50 – 3,00
<b>Mixers</b>		Rolling mill drives	2,00 – 2,50
Constant density	1,75 – 2,25		
Variable density	2,00 – 2,50		

# COUPLING SELECTION BASED ON OPERATING FACTORS

## Coupling selection

The coupling selection is based on operating factors. The coupling has to be dimensioned in a way that the permissible coupling load is not exceeded with any operating condition. For this purpose the actual loads have to be compared to the permissible parameters of the coupling. The shaft-hub-connection has to be investigated by the customer.

### 1. Drives without periodical torsional vibrations

For example centrifugal pumps, fans, screw compressors, etc. The coupling selection requires that the rated torque  $T_{KN}$  and the maximum torque  $T_{Kmax}$  are received.

#### 1.1 Loading by rated torque

Taking into account the operating factor  $S_B$ , the temperature factor  $S_t$  and the directional factor  $S_R$ , the permissible rated torque must

$$T_N [Nm] = 9550 \cdot \frac{P [kW]}{n [1/min]}$$

$$T_{KN} \geq T_N \cdot S_B \cdot S_t \cdot S_R$$

be at least as big as the the rated torque  $T_N$  of the machine.

#### 1.2 Loading by torque shocks

The permissible maximum torque of  $T_{Kmax}$  of the coupling must be at least as big as the sum of the peak torque  $T_S$  and the rated torque  $T_N$  of the machine, taking into account all relevant service factors. This applies in case that the rated torque of the machine is superimposed by a shock. For drives with A. C. motors and big masses on the load side we would recommend to do a joint calculation of the peak starting torque by our simulation programm.

$$T_{Kmax} \geq (T_N + T_S) \cdot S_Z \cdot S_t \cdot S_R$$

### 2. Drives with periodical torsional vibrations

For drives subject to dangerous torsional vibrations e. g. diesel engines, piston compressors, piston pumps, generators, etc. it is necessary to perform a torsional vibration calculation to ensure a correct coupling selection. KTR is able to perform such a torsional vibration calculation and coupling selection in house. For necessary details please see KTR standard 20004.

# COUPLING SELECTION BASED ON OPERATING FACTORS

## Example of calculation

- Requested:** Double-cardanic steel lamina coupling for bridging a shaft distance dimension → RADEX®-N  
**Application:** Connection of IEC standard motor and radial pump  
 ▪ Coupling selection following page 16, item 1: Drives without periodical torsional vibrations

### Given: Details of driving side

Rotary current motor:	Size 315 L	
Motor output:	P = 200 kW	
Speed:	n = 1500 1/min	
Starting frequency:	6 times per hour	→ S <sub>Z</sub> = 1.0 (see page 15)
Ambient temperature:	+ 65 °C	→ S <sub>t</sub> = 1.0 (see page 15)
Peak torque (starting torque) T <sub>AS</sub>	= 2 • T <sub>AN</sub>	
Diameter of motor shaft	80 mm	

### Given: Details of load side

Radial pump		→ S <sub>B</sub> = 1.5 (see page 15)
Rated torque of load side:	T <sub>LN</sub> = 930 Nm	
Diameter of pump shaft	75 mm	
Distance dimension of motor shaft - pump shaft (DBSE)	= 250 mm	
Direction of torque	same	→ S <sub>R</sub> = 1.0 (see page 15)

### Calculation

#### 1.1 Loading by rated torque

- Rated torque of drive T<sub>AN</sub>

$$T_{AN} = 9550 \cdot \frac{P [\text{kW}]}{n [1/\text{min}]} \quad \rightarrow 9550 \cdot \frac{200 \text{ kW}}{1500 1/\text{min}} = 1273 \text{ Nm}$$

- Load produced by rated torque

$$T_{KN} \geq T_{AN} \cdot S_B \cdot S_t \cdot S_R \quad \rightarrow 1273 \text{ Nm} \cdot 1,5 \cdot 1 \cdot 1 = 1909,5 \text{ Nm} \quad \rightarrow T_{KN} \geq 1909,5 \text{ Nm}$$

#### 1.2 Loading by torque shocks

- Shock on driving side without load torque being overlapping

$$T_{K \text{ max.}} \geq (T_N + T_S) \cdot S_Z \cdot S_t \cdot S_R \quad \rightarrow T_N = 0$$

$$\quad \rightarrow \text{Starting torque } T_{AS} = 2 \cdot T_{AN} \quad \rightarrow 2 \cdot 930 \text{ Nm} = 1860 \text{ Nm}$$

$$\rightarrow T_{K \text{ max.}} \geq 1860 \text{ Nm} \cdot 1 \cdot 1 \cdot 1 = 1860 \text{ Nm}$$

- Coupling selection

$$T_{KN} = 2400 \text{ Nm}$$

$$T_{K \text{ max.}} = 4800 \text{ Nm}$$

### Result

The coupling is sufficiently dimensioned.

### Please note:

The shaft-hub-connection has to be verified by the customer separately.